

Hidden Quarry

Rockwood Ontario

Prepared for:

James Dick Construction Limited

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19 November 2012

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1 Introduction

Aercoustics Engineering Limited has been retained by James Dick Construction Limited to carry out an environmental noise impact study for the subject quarry in the Township of Guelph-Eramosa, Ontario.

The purpose of this study is to assess the noise impact of the proposed quarry on the neighbouring residences. It has been prepared in accordance with the Aggregate Resources Act requirement for noise assessment. An area location map is given in Figure 1 which illustrates the designated calculation locations for processing noise (i.e. R1 through R19). An operational plan is shown in Figure 2A and 2B which identifies the extraction boundaries, phasing, equipment locations, and proposed direction of extraction.

2 Background Information

The background information used in evaluating the noise impact of this quarry is taken from the Aercoustics Engineering Limited database which comprises information obtained from acoustic performance measurement surveys conducted for numerous processing plants, pits, and quarries throughout Ontario. The proposed equipment type and operation is similar to a number of other sites such as the Rockfort Quarry which is also owned and operated by James Dick Construction Limited. In order to assess the noise and vibration impact of the proposed quarry, it was necessary to conduct site and terrain specific noise modelling of work patterns, phasing and proposed equipment operation. Operation of peak period activity under both start-up conditions and operation at the extraction limits were modelled at the designated calculation locations identified in this study.

Site-specific information pertaining to this proposed quarry is as follows:

1. The proposed hours of full operation are normally:
 - 0600-1800 hours for shipping
 - 0700-1900 for drilling, processing, and extraction
2. The quarry extraction stages will be phased as shown in Figure 2A and 2B, with sand and gravel extraction occurring during Stage 1, and dolomite extraction occurring in Stage 2.
3. The operation will entail the use of the following equipment:
 - processing plant, crusher, screens, wash plant (700,000 tonnes per year)
 - delivery trucks
 - 1 extraction front end loader
 - 1 sales/shipping loader
 - 1 dragline (8 yard)

- 1 hydraulic drill
- Bulldozer/backhoe/scrapper for site preparation and construction
- 3 rock trucks.

4. There are no fish spawning beds in the vicinity of the quarry.

3 Criteria and Guidelines

The noise impact methodology used in this study is based on sound and vibration impact guidelines stipulated by MOE in publications NPC-205/232/233, and the Aggregate Resources Act. MOE publication NPC-115 has also been referenced accordingly in order to address construction noise due to site preparation activities such as berm construction. The MOE Guidelines for noise and vibration impact are included in Appendix A of this report.

In addition, ISO standard 9613-2 on sound propagation outdoors has been used to further substantiate the environmental noise assessment presented in this study.

3.1 Ambient Noise Assessment

The existing noise environment comprises mostly natural sounds, as well as road traffic noise on Highway 7, 6th Line and 5th Line. The sound level criteria at points of reception are set by the guidelines in MOE publications NPC-205/232. According to these publications, the applicable sound level limit is the greater of the lowest 1-hour Leq measured at the critical receptor or the MOE defined limit for that class designation.

Nineteen sensitive points of reception have been identified surrounding the proposed Quarry. The locations and assigned ID#s for each receptor are labelled in the Figure 1 Area Location Map.

Receptors R1, R2, R10, and R12 to R16 are exposed to elevated levels of traffic noise from Highway 7. These receptors are considered to exist in a Class 2 area, as defined by the MOE, while all others are considered to exist in a Class 3 area. Receptor classes are summarized in the following table:

Table 1: Summary of Receptor Classes

Receptor ID	R1	R2	R3	R4	R5	R6	R7	R8	R9	R10	R11	R12	R13	R14	R15	R16	R17	R18	R19
MOE Acoustical Class 2	•	•								•		•	•	•	•				
MOE Acoustical Class 3			•	•	•	•	•	•	•		•						•	•	•

Daytime performance limits have been established for some of these receptors based on STAMSON prediction calculations, using Ministry of Transportation (MTO) annual average daily traffic (AADT) volume data from 2007. The predicted daytime background noise level due to Highway 7 traffic at these receptors is given in Table 2. Sample calculations are provided in Appendix C.

Table 2: Daytime Performance Limit Summary for Class 2 Receptors

Receptor ID	Daytime (07:00-19:00) Performance Limit (dBA)
R2	51
R10	53
R14	53
R16	57

The applicable sound level performance limit for each receptor is summarized in Table 3:

Table 3: Summary of Sound Level Performance Limits for All Receptors

Receptor ID	Daytime (07:00-19:00) dBA	Evening (19:00-23:00) dBA	Night time (19:00-07:00) dBA
R1	50	45	45
R2	51	45	45
R3	45	40	40
R4	45	40	40
R5	45	40	40
R6	45	40	40
R7	45	40	40
R8	45	40	40
R9	45	40	40
R10	53	45	45
R11	45	40	45
R12	50	45	45
R13	50	45	45
R14	53	45	45
R15	50	45	45
R16	57	45	45
R17	45	40	40
R18	45	40	40
R19	45	40	40

The receptor height used for calculation purposes is 1.5m above the receptor area grade.

3.2 Construction and Site Preparation/Rehabilitation Noise

Construction and site preparation/rehabilitation activities will be occurring during various stages of quarrying and will include activities such as site clearing and berm construction. These activities will occur as preparation for the various stages of the operation.

These activities are considered to be exempt from satisfying the MOE stationary noise source guidelines (i.e., 'non-stationary' noise source); namely publication NPC-205/232. All construction equipment must meet the sound emission standards defined in MOE publication NPC-115. The relevant background information on non-stationary noise sources as well as publication NPC-115 is

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given in MOE Model Municipal Noise Control Bylaw, 1978 as well as the sound source exclusions defined in MOE publications NPC 205/232, 1995, included in Appendix A.

4 Recommendations

The following recommendations are provided in order to meet the applicable criteria:

- 12m and 10m high stockpiles should be maintained in certain locations around the processing plant for each phase and stage. The stockpile peaks should be located no further than 30m from the processing plant, and should be located such that, in plan, they block line-of-sight between processing plant equipment and sensitive receptors, as described in the table below:

Table 4: Recommended Stockpile Height and Position

Stockpiles Positioned to Shield Receptor IDs	Minimum Stockpile Height (m)
R1, R15, R16, R17, R18	10
R3, R4, R5, R11, R19	12

This configuration is illustrated on Figure 3.

- A quiet drill with a maximum sound power rating of 112dBA should be used. This corresponds to a maximum sound pressure level rating of 75dBA at 30 meters.
- Earth berms should be constructed to the elevations shown and located as shown on Figure 3.
- The recommended direction of extraction is indicated on Figure 3.
- The permanent processing plant area should be established at an elevation of 349m, and a haul route trench connecting the processing plant area to the Stage 1 Phase 1 extraction area should be excavated to the same 349m elevation.
- All construction equipment used in site preparation/construction must meet the sound emission standards defined in MOE publication NPC-115. The relevant background information on non-stationary noise sources as well as publication NPC-115 is given in MOE Model Municipal Noise Control Bylaw, 1978 as well as the sound source exclusions defined in MOE publications NPC 205/232, 1995, included in the attached.

5 Noise Level Predictions

The general operation of the proposed quarry is discussed in Section 2.0. Equipment sound power levels and source heights are listed in Table 5 and are based on information in the Aercoustics Engineering Limited pits and quarries noise emission database.

Table 5: Summary of Stationary Source Sound Power Levels

Source ID	Source Description	Sound Power Level (dBA)	Effective Source Height (m)
S1	Processing Plant	123	3
S2	Shipping Loader	107	2.5
S3	Drill	112	1.5
S4	Shipping Truck	103	1.5
S5	Extraction Loader	107	2.5
S6	Quarry Truck	112	2.5

From this information, the source to receptor geometry can be established in order to facilitate noise level calculations and design any mitigation measures such as shielding berms and stockpiles.

The noise impact prediction calculations were performed using the DataKustik CadnaA environmental noise prediction software. The calculations are based on established prediction methods; ISO 9613-2: A Standard for Outdoor Noise Propagation standard. The noise impact predictions assumed downwind propagation conditions as defined by the standard.

Table 6 shows a summary of impacts that are predicted to occur with the implementation of recommendations given in Section 4 of this report.

Table 6: Summary of Predicted Impacts

Receptor ID	Time Period	Worst Case Impact From Source							Overall (dBA)	Limit (dBA)
		Processing Plant (dBA)	Shipping Loader (dBA)	Shipping Truck (dBA)	Extraction Loader (dBA)	Rock Trucks (dBA)	Drill (dBA)			
R1	Day	43	33	25	34	33	34	45	50	
	Night	N/A	33	25	N/A	N/A	N/A	34	45	
R2	Day	46	31	22	32	31	32	47	51	
	Night	N/A	31	22	N/A	N/A	N/A	31	45	
R3	Day	36	20	26	39	39	40	43	45	
	Night	N/A	20	26	N/A	N/A	N/A	27	40	
R4	Day	35	19	22	35	35	36	40	45	
	Night	N/A	19	22	N/A	N/A	N/A	24	40	
R5	Day	34	17	20	36	36	35	40	45	
	Night	N/A	17	20	N/A	N/A	N/A	22	40	
R6	Day	39	15	13	28	30	30	40	45	
	Night	N/A	15	13	N/A	N/A	N/A	16	40	
R7	Day	39	24	14	29	30	30	40	45	
	Night	N/A	24	14	N/A	N/A	N/A	24	40	
R8	Day	39	24	15	30	30	31	41	45	

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Receptor ID	Time Period	Worst Case Impact From Source							Overall (dBA)	Limit (dBA)
		Processing Plant (dBA)	Shipping Loader (dBA)	Shipping Truck (dBA)	Extraction Loader (dBA)	Rock Trucks (dBA)	Drill (dBA)			
R9	Night	N/A	24	15	N/A	N/A	N/A	24	40	
	Day	40	25	16	31	31	32	41	45	
R10	Night	N/A	25	16	N/A	N/A	N/A	25	40	
	Day	46	31	20	36	36	38	48	53	
R11	Night	N/A	31	20	N/A	N/A	N/A	31	45	
	Day	35	19	23	37	37	37	41	45	
R12	Night	N/A	19	23	N/A	N/A	N/A	24	40	
	Day	46	31	22	36	37	41	48	50	
R13	Night	N/A	31	22	N/A	N/A	N/A	32	45	
	Day	43	29	18	37	40	45	48	50	
R14	Night	N/A	29	18	N/A	N/A	N/A	30	45	
	Day	47	31	19	35	36	37	48	53	
R15	Night	N/A	31	19	N/A	N/A	N/A	31	45	
	Day	42	29	24	37	35	37	44	50	
R16	Night	N/A	29	24	N/A	N/A	N/A	30	45	
	Day	46	38	25	38	34	38	48	57	
R17	Night	N/A	38	25	N/A	N/A	N/A	38	45	
	Day	37	25	19	31	31	32	40	45	
R18	Night	N/A	25	19	N/A	N/A	N/A	26	40	
	Day	41	29	25	34	33	34	43	45	
R19	Night	N/A	29	25	N/A	N/A	N/A	30	40	
	Day	35	19	23	39	39	39	43	45	
	Night	N/A	19	23	N/A	N/A	N/A	24	40	

Note: The listed noise levels represent the maximum predicted impact for each individual source, and the overall. It should be noted that the overall may not equal the sum of the source maximums, as each maximum may not occur concurrently (i.e during different stages or phases).

Sample calculations are given in Appendix C.

With the mitigation recommended the impacts at each sensitive point of reception are predicted to satisfy the applicable MOE limits.

6 Conclusions

Aercoustics Engineering Limited has been retained by James Dick Construction Limited to carry out an environmental noise impact study for the subject quarry in the Township of Guelph-Eramosa, Ontario.

Receptor locations have been identified, and criteria have been established for each. Recommendations have been provided which include the implementation and enforcement of stockpile, earth berm, and direction of extraction requirements, pneumatic drill sound level limitations, and processing plant positioning requirements.

With the implementation of these recommendations, it has been demonstrated that the applicable criteria are satisfied.

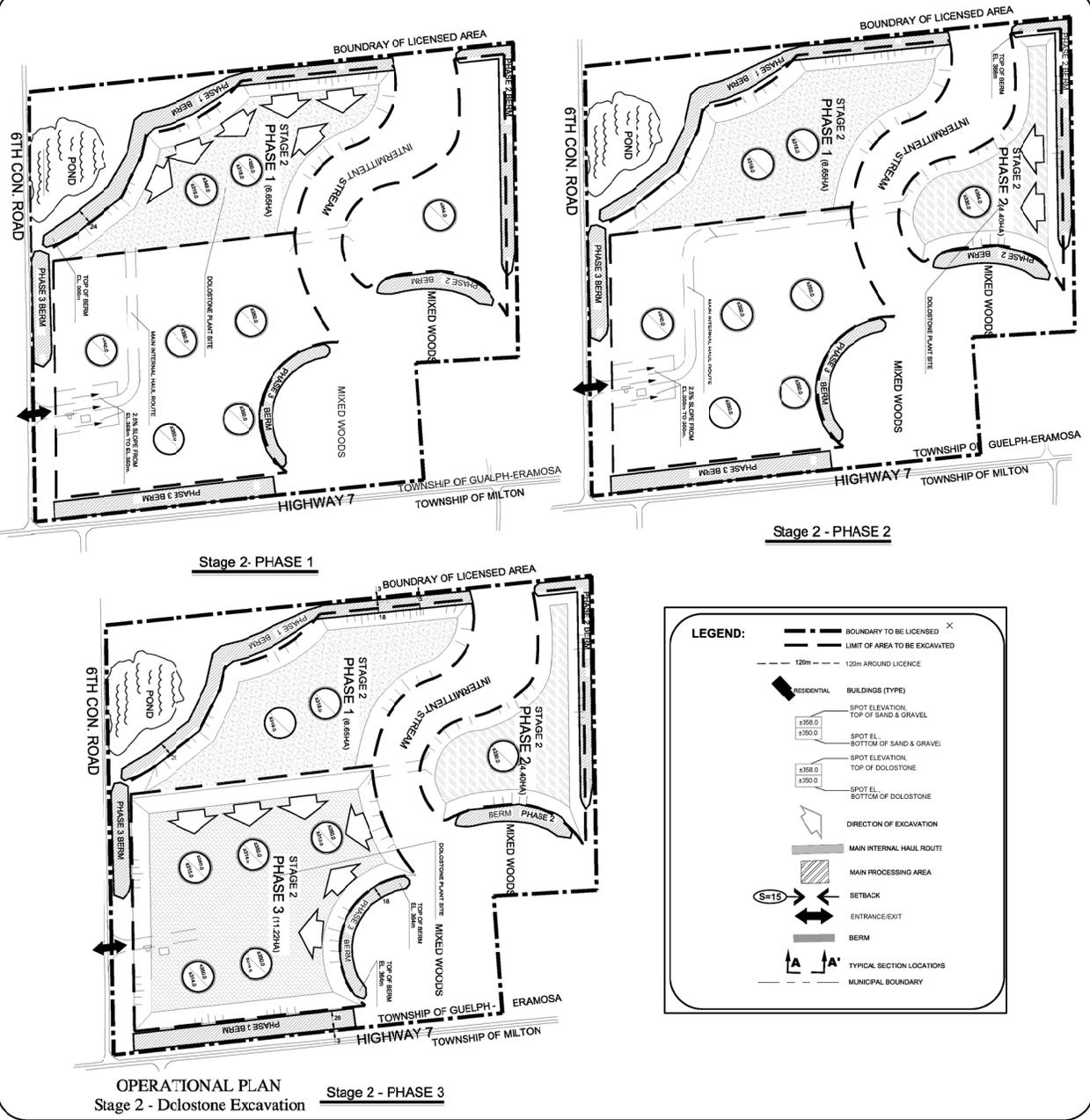


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Eramosa Quarry
Figure 1: Area Location Map

Drawn DG	Eng. VG	Drawing Area Location Map	
The scope of the work outlined in this document is limited to the acoustic noise & vibration control aspects of the design. Contractor to verify all dimensions.		Scale AS SHOWN	Figure 1



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Eramosa Quarry
Figure 2B: Stage 2 Site Plan

Drawn
DG

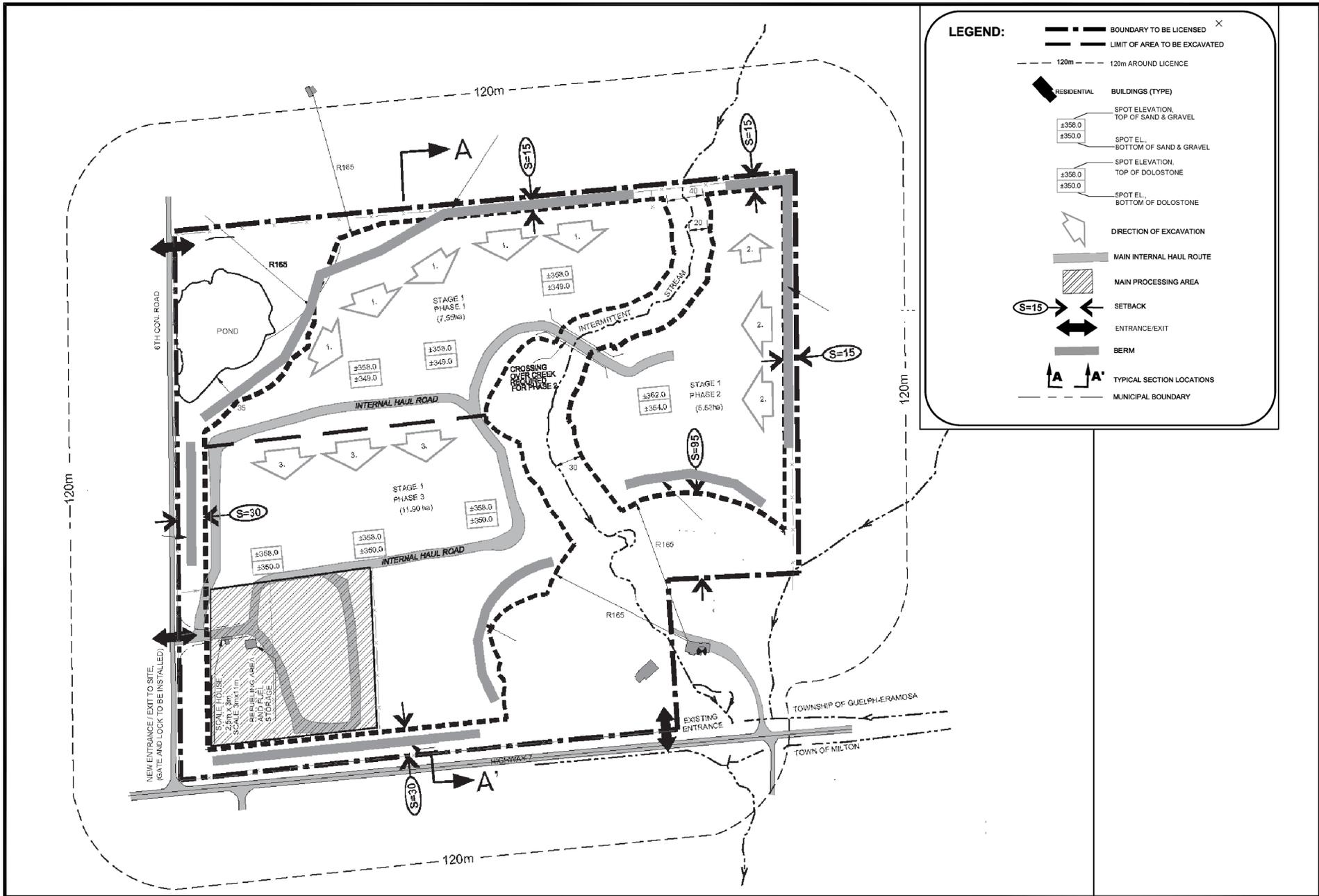
Eng.
VG

Drawing
S2 Site Plan

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Scale
AS
SHOWN

Figure
2B



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Eramosa Quarry
Figure 2A: Stage 1 Site Plan

Drawn
DG

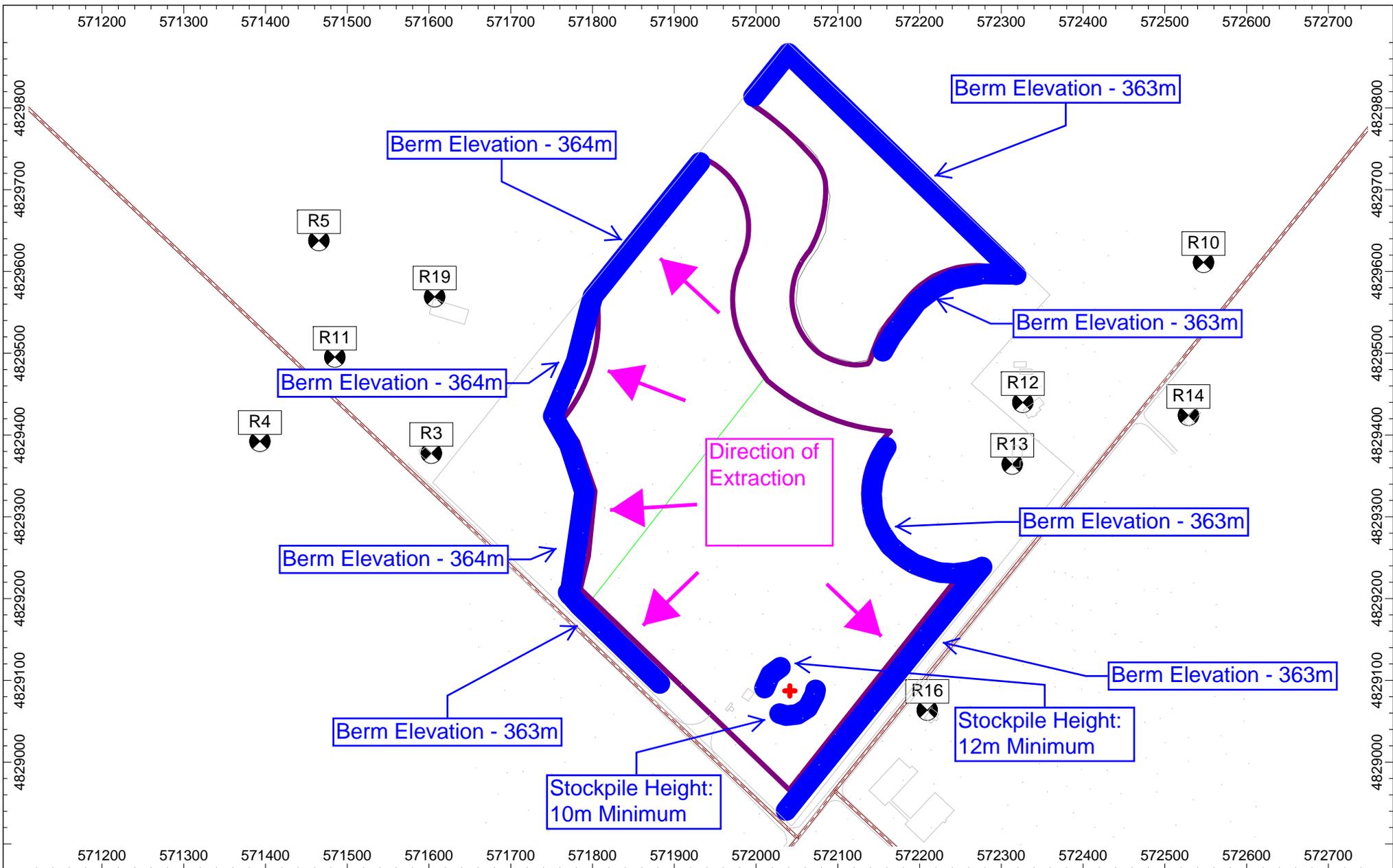
Eng.
VG

Drawing
S1 Site Plan

The scope of the work outlined in this document is limited to the acoustic noise & vibration control aspects of the design. Contractor to verify all dimensions.

Scale
AS
SHOWN

Figure
2A



Scale: NTS
 Drawn: DG
 Eng: VG
 Date: Jul 13, 2012

The scope of the work outlined in this document is limited to the acoustic, noise, and/or vibration control aspects of the design. Contractors to verify all dimensions

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Project:
 Eramosa Quarry

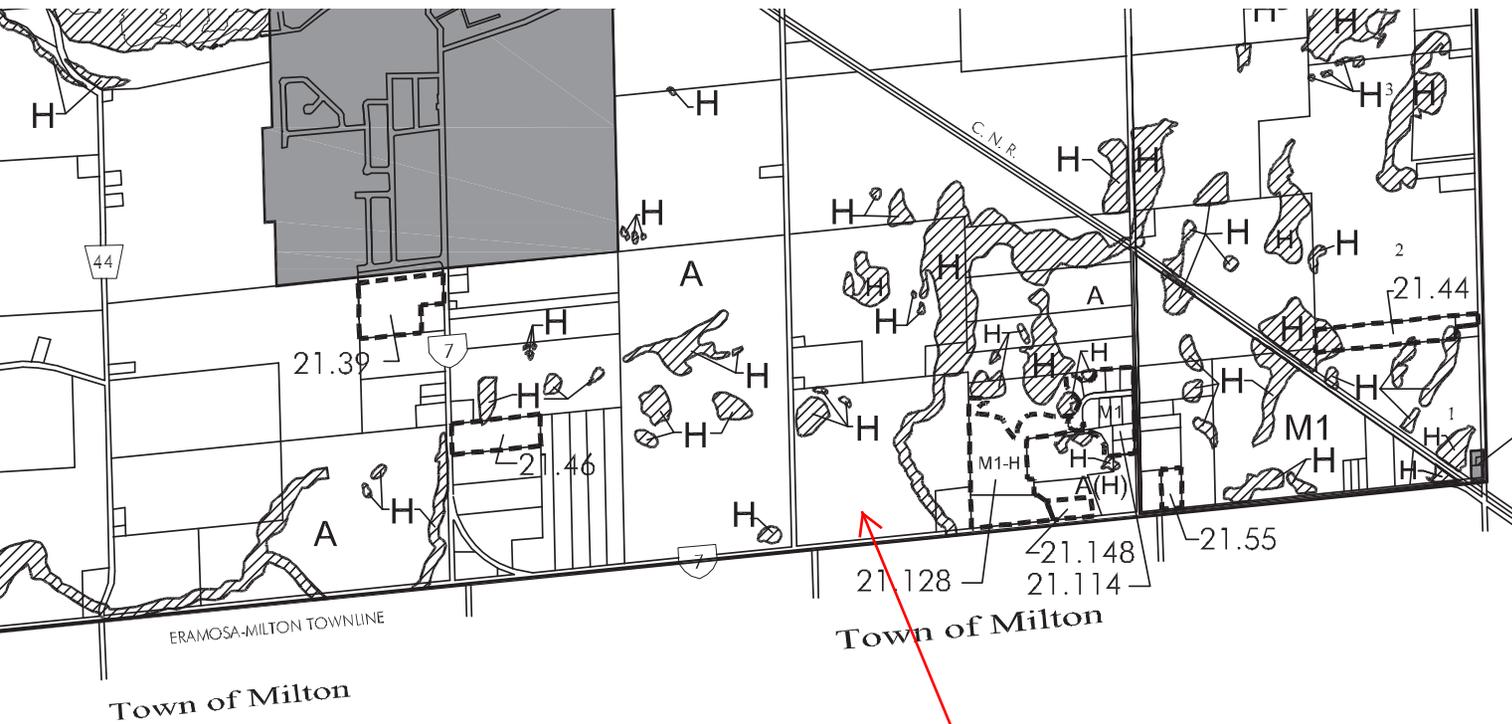
Drawing Title:
 Recommended Noise Controls

Project Number: 11107

Figure: 3

Appendix A

Zoning Map



CREWSONS
CORNERS

LEGEND

- A Agricultural
- R1 Village Residential Low Density
- R2 Village Residential Medium Density
- RR Rural Residential
- C1 Village Commercial
- C2 Village Service Commercial
- C3 Hamlet Mixed Use
- C4 Highway Commercial
- I Institutional
- M1 Rural Industrial
- M2 Agricultural Business
- M3 Extractive Industrial
- M4 Disposal Industrial
- OS Open Space
-  Hazard
-  Special Provisions

NOTE: THIS SCHEDULE TO BE READ IN CONJUNCTION
WITH APPLICABLE SECTIONS OF THE BY-LAW.

CONSOLIDATED TO DECEMBER 31, 2009

Appendix B

Sound Power Data

Name	63	125	250	500	1000	2000	4000	8000	A	lin
Processing Plant	114	117	121	119	119	116	110	100	123	126
Cat 980H	118	113	106	102	101	100	91	93	107	120
Drill	122	114	107	104	105	106	103	98	112	124
Rock Truck passby at 30km/hr	108	109	110	109	108	106	101	97	112	117
Highway Truck (25 kph)	106	100	98	100	100	96	88	78	103	111

Appendix C

Sample Calculations

ISO 9613-2 Sample Calculation

Receiver: R3

Project: Hidden Quarry

Project Number: 11007

Time Period	Total (dBA)
Day	43
Night	27

Receiver Name	Receiver ID	X	Y	Z	Ground
R3	R3	571603	4829378	360.8	359.3

Source Name	Source ID	X	Y	Z	Ground	RefIOrd	LxT	LxN	L/A	Dist.	hm	Freq	Adiv	KOb	Agr	Abar	z	Aatm	Afol	Ahou	Cmet	CmetN	Dc	RL	LtotT	LtotN
Processing Plant	A01_S1	572041	4829087	352.0	349	0	123	-1	1.0	526	9.4	0	65.4	0	2.1	16.9	1.3	2.5	0.0	0.0	0.0	0.0	0.0	0.0	36	-88
Shipping Loader	A01_S2	572035	4829097	351.5	349	0	107	107	1.0	515	9.4	0	65.2	0	1.0	18.0	2.2	2.2	0.0	0.0	0.0	0.0	0.0	0.0	20	20
Drill	D09_S3	571897	4829455	351.5	350	0	112	-11	1.0	304	5.4	0	60.7	0	0.7	8.1	0.4	2.5	0.0	0.0	0.0	0.0	0.0	0.0	40	-82
Extraction Loader	D09_S2	571872	4829454	352.5	350	0	107	-1	1.0	280	5.3	0	59.9	0	1.9	6.6	0.4	1.4	0.0	0.0	0.0	0.0	0.0	0.0	37	-70
Shipping Truck	A01_S4	571986	4829098	350.5	349	0	94	94	71.8	475	6.6	0	64.5	0	0.3	5.0	0.3	2.1	0.0	0.0	0.0	0.0	0.0	0.0	22	22
Rock Trucks	D09_S5	571815	4829237	352.5	350	0	97	-16	40.4	255	5.8	0	59.1	0	5.6	10.3	1.4	1.6	0.0	0.0	0.0	0.0	0.0	0.0	20	-93
Rock Trucks	D09_S5	571837	4829303	352.5	350	0	101	-13	99.0	246	5.8	0	58.8	0	4.9	10.1	1.2	1.5	0.0	0.0	0.0	0.0	0.0	0.0	25	-88
Rock Trucks	D09_S5	571868	4829397	352.5	350	0	101	-13	99.0	265	5.7	0	59.5	0	2.5	8.5	0.6	1.6	0.0	0.0	0.0	0.0	0.0	0.0	28	-85
Rock Trucks	D09_S5	571926	4829108	351.5	349	0	101	-12	101.4	421	6.9	0	63.5	0	1.4	4.7	0.3	2.3	0.0	0.0	0.0	0.0	0.0	0.0	29	-84
Rock Trucks	D09_S5	571852	4829178	351.5	349	0	101	-12	101.4	320	6.3	0	61.1	0	2.7	8.3	0.7	1.9	0.0	0.0	0.0	0.0	0.0	0.0	27	-86
Shipping Truck	A01_S4	571944	4829045	361.5	360	0	88	88	16.2	477	4.8	0	64.6	0	3.8	1.8	0.0	2.1	0.0	0.0	0.0	0.0	0.0	0.0	15	15
Shipping Truck	A01_S4	571938	4829037	361.5	360	0	82	82	4.1	478	4.8	0	64.6	0	3.2	1.0	0.0	2.1	0.0	0.0	0.0	0.0	0.0	0.0	11	11
Shipping Truck	A01_S4	571933	4829031	361.5	360	0	86	86	11.7	479	3.4	0	64.6	0	2.5	0.0	0.0	2.1	0.0	0.0	0.0	0.0	0.0	0.0	17	17
Shipping Truck	A01_S4	571957	4829061	356.0	354.5	0	90	90	25.7	475	8.0	0	64.5	0	0.4	4.3	0.1	2.1	0.0	0.0	0.0	0.0	0.0	0.0	18	18
Shipping Truck	A01_S4	572015	4829120	350.5	349	0	88	88	18.0	486	6.5	0	64.7	0	0.2	5.0	0.3	2.2	0.0	0.0	0.0	0.0	0.0	0.0	16	16
Rock Trucks	D09_S5	572012	4829094	351.5	349	0	97	-16	47.0	498	9.6	0	65.0	0	0.7	23.3	9.3	2.6	0.0	0.0	0.0	0.0	0.0	0.0	6	-107
Rock Trucks	D09_S5	571978	4829090	351.5	349	0	97	-16	44.1	473	7.1	0	64.5	0	1.0	4.2	0.2	2.5	0.0	0.0	0.0	0.0	0.0	0.0	25	-88
Rock Trucks	D09_S5	571812	4829215	352.0	349.5	0	90	-23	8.1	265	5.8	0	59.5	0	5.6	10.4	1.5	1.6	0.0	0.0	0.0	0.0	0.0	0.0	13	-100



Appendix D

CVs

credentials + experience

- performed work to support noise impact feasibility studies for several major **Mattamy Homes** housing developments while working at an acoustical consulting firm.
- joined Aercoustics in April 2008 as a noise and vibration consultant.
- involved in environmental compliance projects for several pits and quarries, including **Devon Pit, Hendrik's Quarry, and Flamboro Dufferin Aggregate Quarry**.
- responsible for several environmental compliance projects for a range of industrial/commercial facilities including **Décor Precast, IBM Canada, HP Canada, Royal Bank of Canada, Canadian Tire, and Bell Canada**.
- performed field sound transmission class (FSTC) testing for the **Waterloo Police** as part of a study to determine architectural noise control solutions that address speech-privacy concerns relating to inmate interrogation.
- involved in architectural noise control for a call center at an **HP Canada** datacenter facility.
- involved in several studies to document and provide recommendations for rail vibration measurements for the **Toronto Transit Commission**, as well as measuring and considering subway vibration and streetcar noise.
- performed supporting noise and vibration prediction modeling for several **Toronto Transit Commission** Environmental Assessments.
- jazz pianist, recording studio operator, and avid volleyball player.
- B.A.Sc., Electrical Engineering, Queen's University, 2006

credentials + experience

- first worked for Pratt & Whitney, testing and analyzing gas turbine engine components and aircraft structures for noise and vibration control.
- as a consulting engineer expanded expertise to environmental noise and vibration assessment, noise control design, finite element analysis, structural vibration and machinery dynamics.
- became one of four principals of Aercoustics Engineering Limited in 1992.
- notable projects include one of the world's first outdoor Active Noise Cancellation systems for the **TransAlta** cogeneration facility near the Ottawa Health Sciences Centre – landed an **Award of Excellence** from the Association of Consulting Engineers of Canada; noise assessment and noise control review for the Millbank ABB GT11N Combustion Turbine Generating Station for **New Brunswick Power**; noise assessment for conversion of the Rolls Royce RB211 gas turbine to the WR21 marine power plant for **Westinghouse**; sound measurement program for the Rolls Royce RB211 on behalf of **Cooper-Rolls Royce** for **TransCanada PipeLines**; specialized loudspeaker transducers for Nortel Networks – in media applications, they created the aural impression of a full soundstage for listeners; acoustics and noise control for Toronto's **Filmport Studio** complex; and a field study of wind machine noise in the Niagara wine region.
- has appeared as an **expert witness** on numerous occasions before the Ontario Energy Board (OEB) and Ontario Municipal Board (OMB) and various Environmental Assessment Review Panels, and court cases.
- designs and manufactures loudspeaker systems for **specialized acoustic applications** ranging from active noise cancellation to sound reinforcement systems – has made extensive use of the National Research Council of Canada's computerized anechoic room facilities to optimize enclosure and filter designs.
- member of the **Canadian Acoustical Association, American Society of Mechanical Engineers, Acoustical Society of America and Audio Engineering Society.**
- B.A.Sc. (Mechanical Engineering), University of Toronto, 1984.